



Wetting patterns estimation in cultivation substrates under drip irrigation

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ABSTRACT

To make an accurate and reasonable estimate of the wetting pattern in cultivation substrates, 36 experimental treatments with two replications were conducted under drip irrigation. An empirical model was suggested to predict the substrate full wetting pattern at different application times for T_1 , T_2 , T_3 and T_4 . The maximum root mean square error and mean error were only 1.37 and 0.72 cm, and 1.22 and 0.71 cm for the wetted radius and depth of the full wetting pattern for T_1 , T_2 , T_3 and T_4 . The proposed model performs well in predicting the full wetting pattern and can be used to operate and manage the irrigation system.

Keywords: Wetted pattern; Wetted radius; Wetted depth; Empirical model; Drip irrigation

1. Introduction

Drip irrigation technology is often preferred over sprinkler and other irrigation methods [1], effective design and management of drip irrigation systems leads to efficient delivery of water to the root zone resulting in increased water use efficiency and improved crop production and quality [2–5]. Knowing the wetted zone pattern around the emitter represents a prerequisite to design irrigation systems as well as to manage water [6,7]. The shape of the wetting pattern, which depends on the emitter flow rate and the applied water volume as well as on the soil type, the wetted radius on the soil surface and the wetted depth in the soil are the main parameters of the wetted soil zone [8–12]; there must be an optimum match between the depth and the width of the wetted pattern and the crop root [13]. Numerical models, analytical models and empirical models have been developed to determine the wetting pattern under drip irrigation [14–17]. Numerical and analytical models usually solve governing flow equations for particular initial and boundary conditions [18], but they require detailed information of meteorology, soil and crop, which restricts their practical applications, while the empirical models benefit from having

fewer parameters and requiring fewer inputs than other models, and are therefore more convenient to be used at the field scale [19,20].

As mentioned above, most of the correlative research were conducted on soil [21–24]. In fact, global agriculture has changed dramatically over the last few decades, and the use of soilless cultures has expanded enormously [25,26]. Research on the wetting pattern in soil provides a good foundation for understanding the wetting pattern in substrates; however, as a result of the substantial differences in physical properties between soil and substrates, an independent research on wetting pattern in cultivation substrates is needed.

The simulation of wetting patterns under drip irrigation systems have been studied using empirical models, but the models can estimate only the wetted radius at the substrates surface and the wetted depth in the substrates [27–29]; however, to our knowledge, only few studies have investigated the substrates wetting patterns and so there is a lack of available models to simulate the full substrate wetting patterns under drip irrigation. Therefore, the objective of this study is to develop an enhanced empirical model to estimate the full wetting pattern under drip irrigation with substrate cultivation.

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2. Materials and methods

2.1. Vinegar residue

Vinegar residue is the solid waste product from vinegar production. It contains large amounts of fiber and is acidic. By artificially adjusting the pH, adding effective microorganism groups, and combining with environmental regulation and control technology in the fermentation process, vinegar residue is transformed into an organic substrate.

2.2. Substrates preparation

Four kinds of vinegar residue substrates were used as growth substrates, T_1 , grind vinegar residue (100%); T_2 , grind vinegar residue (75%) and peat (25%); T_3 , grind vinegar residue (50%) and peat (50%); T_4 , grind vinegar residue (50%), peat (25%) and vermiculite (25%). The physical properties are shown in Table 1.

2.3. Experimental design

A plexiglass container of internal dimensions (40 cm length, 40 cm width and 30 cm depth) was used to monitor the advance of wetting patterns at different times during the experiments. To prevent preferential flow along the container walls, the walls were first treated with glue and substrates to create a course surface, before the substrates were filled into the container.

Experiments were conducted in a greenhouse. The substrate was packed in the container with 5 cm increments to obtain a required bulk density and homogeneous substrate profile. Before packing, the substrate was watered until the intended initial substrate water content was reached. The system includes a water pump with adjustable flow, precision digital pressure gauge, water supply pipeline, drip lines and emitters were used to supply irrigation water. One emitter was selected and inserted into the substrate at the corner of plexiglass container, and other emitters irrigate normally.

To examine the effect of emitter discharge, initial substrate water content and irrigation volume on the substrate wetting pattern, 36 experimental treatments with two replications were conducted in the plexiglass container. The water was applied at a rate of 0.15, 0.35 and 0.5 L/h through an emitter and the different emitter discharges were obtained by changing the irrigation pressure. The irrigation volume could be obtained by multiplying emitter discharge and irrigation duration. Three intended initial water content were 0.16, 0.23 and 0.28 cm³/cm³ for T_1 , T_2 , T_3 and T_4 respectively.

During each experiment, the shape of the wetting patterns was drawn on the plexiglass wall at specified times,

the plexiglass walls were cleaned from the substrate and the wetting patterns were copied using graph papers to read the coordinates of the wetting patterns at the end of the experiment.

2.4. Empirical model description

An empirical model was suggested to estimate the wetted radius and depth of the wetted zone by including the effect of emitter discharge, initial substrate water content, irrigation volume, saturated hydraulic conductivity and the depth of emitter insert into the substrate. The empirical model [9] is as follows:

$$W = A_1 V^{n_1} \left(\frac{Ks\theta}{qz} \right)^{\left(n_1 - \frac{1}{3} \right)} \quad (1)$$

$$D = A_2 V^{n_2} \left(\frac{Ks\theta}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \quad (2)$$

where W is the wetted radius (cm), D is the wetted depth (cm), V is the irrigation volume (L), Ks is the saturated hydraulic conductivity (cm/h), q is the emitter discharge (L/h), z is the depth of emitter insert into the substrate (cm), A_1 and A_2 are constants and n_1 and n_2 are exponents of equation. The model is for predicting the wetted radius on the substrate surface and the wetted depth in the substrate. The wetting pattern under the substrate surface was estimated by an empirical model according to the mass of test and experimental data and as demonstrated in the following empirical equation (Eq. (3)):

$$\rho = a(1 + \cos(\alpha)) + b \quad (3)$$

where ρ is the distance between emitter and wetting front, cm; α is the angle between ρ and W (Fig. 1); a and b are coefficients and can be indicated as follows:

$$a = W - D = A_1 V^{n_1} \left(\frac{Ks\theta}{qz} \right)^{\left(n_1 - \frac{1}{3} \right)} - A_2 V^{n_2} \left(\frac{Ks\theta}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \quad (4)$$

$$b = 2D - W = 2A_2 V^{n_2} \left(\frac{Ksq}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} - A_1 V^{n_1} \left(\frac{Ksq}{qz} \right)^{\left(n_1 - \frac{1}{3} \right)} \quad (5)$$

Table 1
Physical properties of vinegar residue substrates

Substrate	Bulk density, g/cm ³	Total porosity, %	Air-filled porosity, %	Hold water porosity, %	Saturated hydraulic conductivity, cm/h
T_1	0.120	71.5	41.0	30.5	5.04
T_2	0.159	74.1	28.2	45.9	3.21
T_3	0.194	72.8	25.2	47.6	3.02
T_4	0.161	80.1	28.8	51.3	2.82

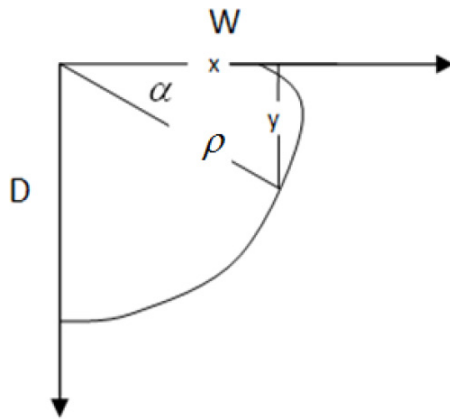


Fig. 1. Cutaway drawing of the wetting pattern.

The horizontal and vertical coordinates of the wetting front can be indicated as follows:

$$y = \left[\left[A_1 V^{n_1} \left(\frac{Ks\theta}{qz} \right)^{\left(n_1 - \frac{1}{3} \right)} - A_2 V^{n_2} \left(\frac{Ks\theta}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \right] \cos(\alpha) + A_2 V^{n_2} \left(\frac{Ksq}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \right] \sin(\alpha) \tag{6}$$

$$x = \left[\left[A_1 V^{n_1} \left(\frac{Ks\theta}{qz} \right)^{\left(n_1 - \frac{1}{3} \right)} - A_2 V^{n_2} \left(\frac{Ks\theta}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \right] \cos(\alpha) + A_2 V^{n_2} \left(\frac{Ksq}{qz} \right)^{\left(n_2 - \frac{1}{3} \right)} \right] \cos(\alpha) \tag{7}$$

where x and y are the wetted radius and wetted depth at a specific application time and any position of the wetting front.

3. Results and discussion

3.1. Variations of wetting pattern under drip irrigation

The wetted radius and depth of the wetting pattern under different emitter discharge, initial water content and irrigation time for T_1 , T_2 , T_3 and T_4 are illustrated in Fig. 2. The wetted radius and depth increased with increasing the irrigation time at the same emitter discharge and initial water content, and with increasing the emitter discharge at the same irrigation time and initial water content; this is due to the matric suction gradient increased with increasing the irrigation volume. The wetted radius increased with increasing the initial water content at the same irrigation time and emitter discharge; however, the maximum wetted depth appeared in the minimum initial water content at the same irrigation time; this is due to the water movement downward was driven mainly by the large porosity of the substrate, the greater gradient of matric suction with lower initial water content, and the gravitational forces.

The coefficients were fitted for the suggested model using the data obtained from the experiments by Microsoft Excel and listed in Table 2.

The performance of the model in predicting the wetting patterns was assessed using the root mean square error (RMSE) and mean error (ME) approaches. The equations are as follows:

$$RMSE = \left[\frac{1}{N} \sum_{i=1}^N (C_{si} - C_{oi})^2 \right]^{1/2} \tag{8}$$

$$ME = \frac{1}{N} \left| \sum_{i=1}^N (C_{si} - C_{oi}) \right| \tag{9}$$

where N is the total number of data, C_{si} is the simulated data, C_{oi} is the observed data and C_o is the mean of the observed data.

It is clear from Table 2 that the proposed model has a good performance between the simulated values and the observed values and from the low values of RMSE and ME. The results are also confirmed by the linear regressions between simulated values and the observed values (Fig. 3). It is obvious from Fig. 3 that all the points have a uniform distribution and a high values of R^2 which indicates a good performance for the proposed model; however, the precision of the model for wetted depth is better than wetted radius because the roughness of substrate surface caused by large granular vinegar residue contained in the substrate, the physical properties of the substrate and the measurement error of the wetted radius. The substrate with highly porous and low bulk density has a poor water holding capacity that results in the smaller wetted radius, and the coarse texture of the substrate surface reduces the horizontal matric suction non-uniform that delays the horizontal advances generally and leads to the difference in length of wetted radius, and the measurement error of the wetted radius, all of these have an impact on the coefficients of the model and reduce the prediction accuracy.

3.2. Estimating the full wetting pattern

Quantitative assessment of the full wetted pattern is essential for optimal irrigation management and important for the determination of the laterals spacing on the substrate surface under drip irrigation, because the maximum wetted radius located at a certain depth under the substrate surface which leads to overlapping between the patterns of adjacent emitters before the surface wetted radii overlapped [8]; however, it is difficult to find a suitable equation to predict the full pattern directly, especially in large granular cultivation substrate. The suggested empirical model enables to predict the wetted radius (W) and wetted depth (D) and a heart-shaped equation (Eq. (3)) was used to estimate the full wetting pattern according to the shape of the wetting pattern below the substrate surface, the coefficients a and b were indicated by the wetted radius (W) and wetted depth (D) as follows from Eqs. (4) and (5), which were obtained depending on the angle at 0° and 90° of Eq. (3). The wetted radius and wetted depth at a specific application time and any position of the wetting front can be indicated by Eqs. (6) and (7).

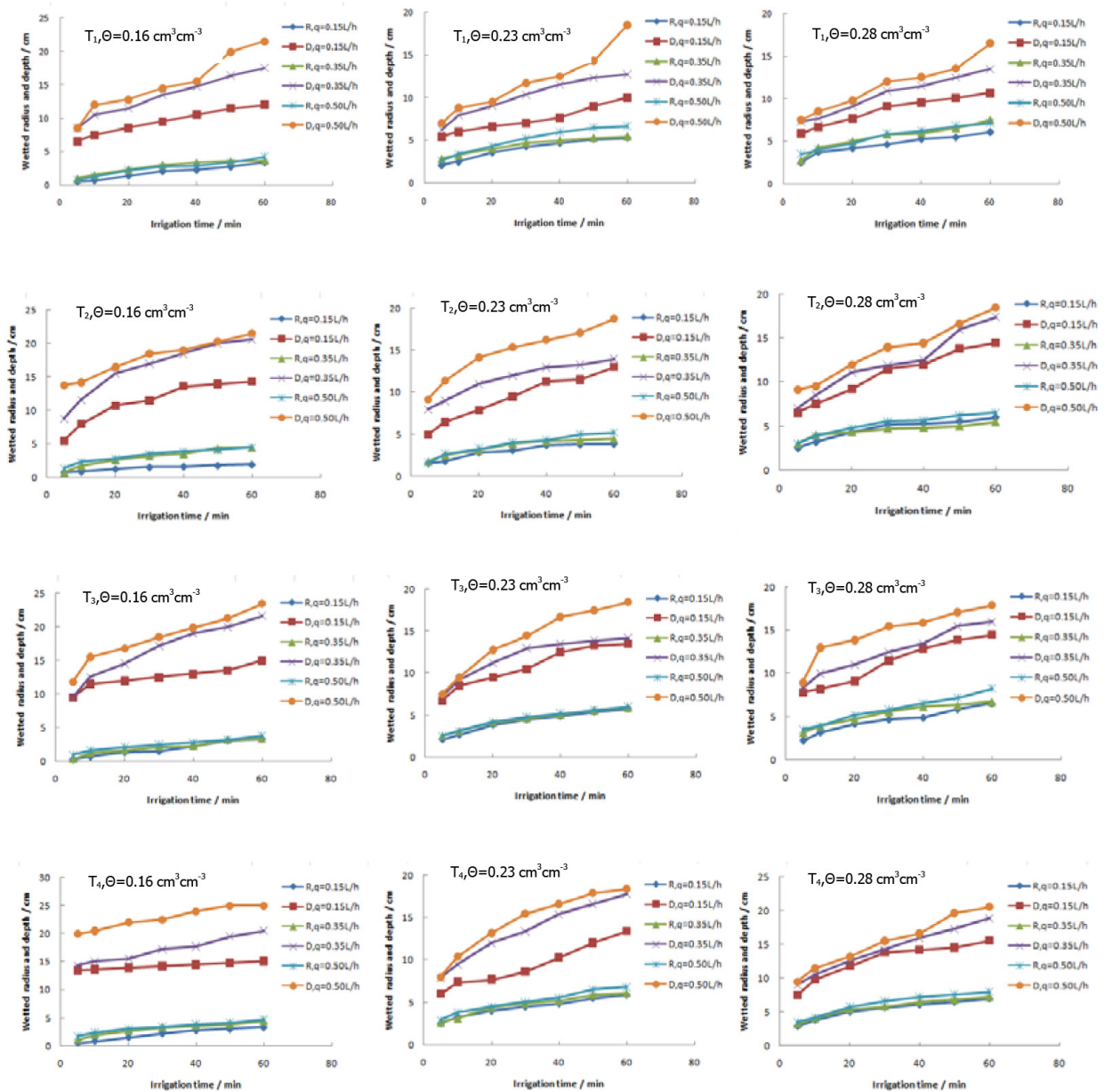


Fig. 2. Wetting pattern variations under different emitter discharge, initial water content and irrigation time for T_1 , T_2 , T_3 and T_4 .

Table 2
Coefficients of the suggested model

Substrate	A_1	n_1	A_2	n_2	RMSE (W/D)	ME (W/D)
T_1	0.379	0.616	2.726	0.216	0.89/0.66	0.19/0.14
T_2	0.384	0.59	2.593	0.307	0.73/0.91	0.13/0.16
T_3	0.151	1.012	2.957	0.277	0.99/1.11	0.35/0.53
T_4	0.615	0.495	2.889	0.279	0.98/0.95	0.05/0.16

Fig. 4 describes the simulated and observed wetted radius and wetted depth of the wetting patterns with 1:1 line at different depth in the substrate and different application times for T_1 , T_2 , T_3 and T_4 under different irrigation condition, the simulated and observed wetted radius and wetted depth of the wetting patterns at 0° (the wetted radius on substrate

surface) and 90° (the maximum wetted depth) are described in Fig. 3. It is clear that there is a good agreement between the simulated values and the observed values, the RMSE and ME were used to verify the model performance and the values are shown in Table 3, the maximum RMSE and ME were only 1.37 and 0.72 cm and 1.22 and 0.71 cm for the wetted

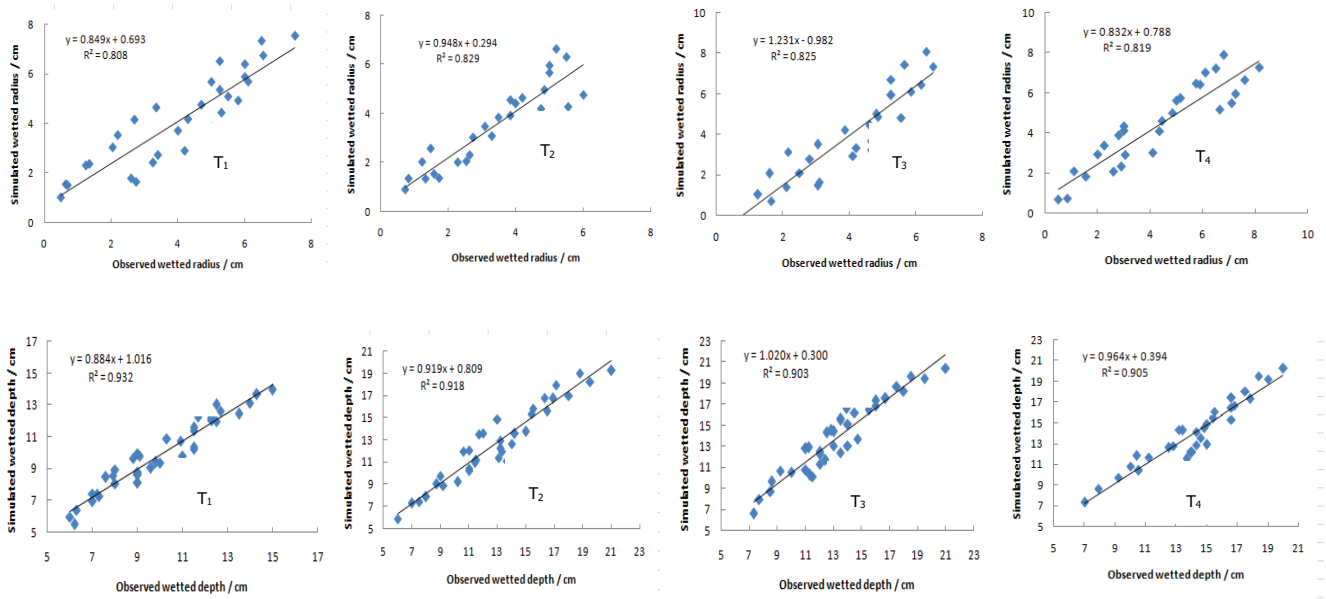


Fig. 3. Simulated and observed wetted radius and wetted depth for T_1 , T_2 , T_3 and T_4 .

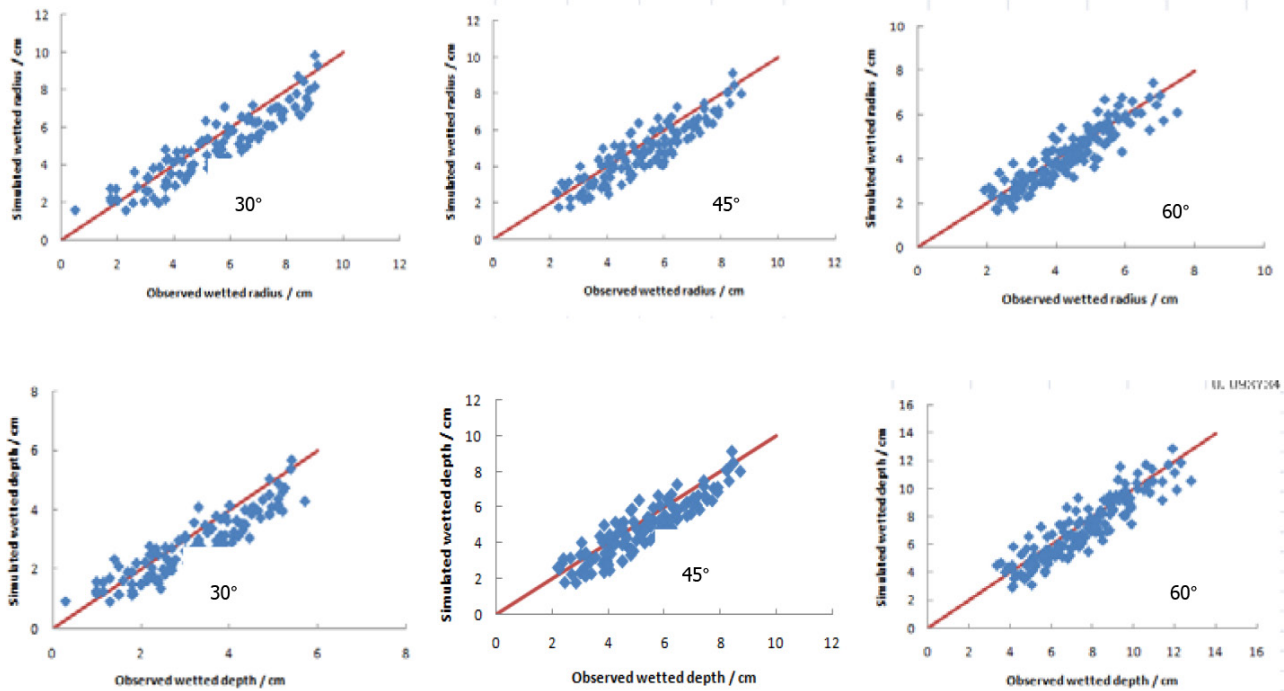


Fig. 4. Simulated and observed wetted radius and wetted depth at different depth and different application times for T_1 , T_2 , T_3 and T_4 .

Table 3
RMSE and ME of the suggested model for wetting pattern

Substrate	30°		45°		60°	
	RMSE (W/D)	ME (W/D)	RMSE (W/D)	ME (W/D)	RMSE (W/D)	ME (W/D)
T_1	1.37/0.66	0.29/0.39	0.83/0.91	0.71/0.71	0.42/0.66	0.22/0.50
T_2	0.94/0.48	0.29/0.42	0.99/0.63	0.09/0.11	0.85/0.48	0.11/0.04
T_3	1.04/0.72	0.27/0.54	0.60/1.02	0.63/0.66	0.62/0.72	0.07/0.29
T_4	1.09/0.77	0.63/0.33	0.88/0.95	0.58/0.61	0.75/0.77	0.39/0.76

radius and depth of the full wetting pattern for T_1 , T_2 , T_3 and T_4 . Therefore the proposed model can be used to calculate the wetting pattern and design the drip irrigation system.

4. Conclusion

36 experimental treatments with two replications were conducted under drip irrigation using three emitter discharges, four type of substrates and three substrate initial water content in this paper. An empirical model, which included emitter discharge, substrate initial water content, irrigation volume, saturated hydraulic conductivity and the depth of emitter insert into the substrate, was suggested to predict the substrate wetted radius and depth as well as estimating the wetting pattern at different depth in the substrate and different application times for T_1 , T_2 , T_3 and T_4 . The performance of the model in predicting the wetting patterns was assessed using the RMSE and ME approaches in replicating experimental data in different conditions, and the maximum RMSE and ME were only 1.37 and 0.72 cm, and 1.22 and 0.71 cm for the wetted radius and depth of the full wetting pattern for T_1 , T_2 , T_3 and T_4 . The results obtained from this study would be useful for design, operation and management of the drip irrigation system.

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